

TMD example of a high-rise building (20-story model)

1. Building Model

- 20 story steel building (lumped mass model with shear spring)
- Story height 3.2 m
- Building height $H = 3.2 \text{ m} \times 20 = 64 \text{ m}$
- Natural period $T = 0.02 H = 1.28 \text{ sec}$
- Plan size X direction: 20 m, Y-direction: 28 m
- Story weight Assuming the unit weight 12 kN/m^2 , $W_i = 6720 \text{ kN}$
- Story mass $M_i = \frac{W_i}{g} = \frac{6720 \text{ kN}}{9.806 \times 10^3 \text{ mm/s}^2} = 0.6853 \text{ kN} \cdot \text{s}^2 / \text{mm}$
- Building mass $M_s = \frac{W_s}{g} = \frac{134.4 \times 10^3 \text{ kN}}{9.806 \times 10^3 \text{ mm/s}^2} = 13.71 \text{ kN} \cdot \text{s}^2 / \text{mm}$
- Story stiffness From the Appendix

$$k_i = \frac{1}{2} [n(n+1) - i(i-1)] m_i \omega^2 \quad i = 1 \text{ to } n$$

- Story damping Assuming the proportional damping to the stiffness

$$c_i = 2h\omega \frac{k_i}{\omega^2} = \frac{2h}{\omega} k_i = \alpha k_i, \quad \alpha = \frac{2h}{\omega}$$

where h is the damping factor (=0.02)

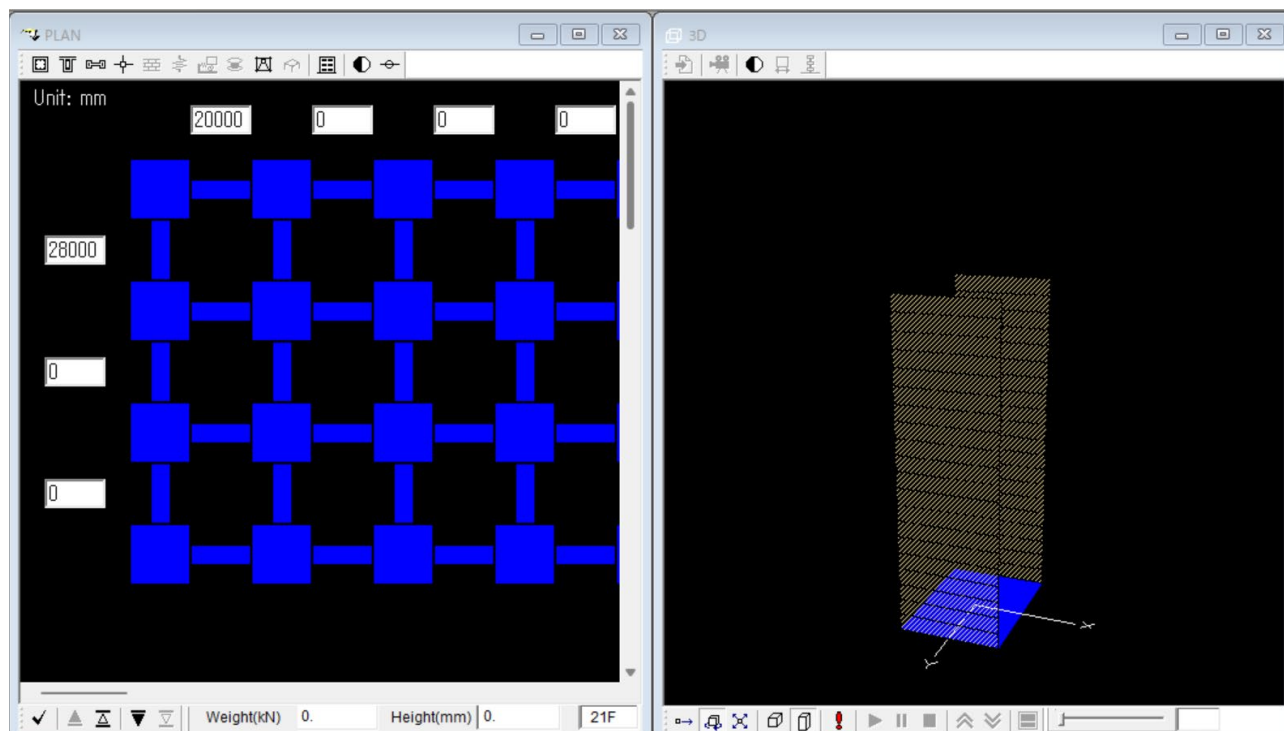


Figure 1 Analysis model of the building (20-story model without TMD.stera)

Table 1 Properties of Building

Story	Height (mm)	Weight (kN)	K (kN/mm)	C (kN.s/mm)
1	3200	6720	3467.7	28.3
2	3200	6720	3451.1	28.1
3	3200	6720	3418.1	27.9
4	3200	6720	3368.6	27.4
5	3200	6720	3302.5	26.9
6	3200	6720	3220.0	26.2
7	3200	6720	3120.9	25.4
8	3200	6720	3005.3	24.5
9	3200	6720	2873.2	23.4
10	3200	6720	2724.6	22.2
11	3200	6720	2559.5	20.9
12	3200	6720	2377.8	19.4
13	3200	6720	2179.7	17.8
14	3200	6720	1965.0	16.0
15	3200	6720	1733.8	14.1
16	3200	6720	1486.1	12.1
17	3200	6720	1221.9	10.0
18	3200	6720	941.2	7.7
19	3200	6720	644.0	5.2
20	3200	6720	330.3	2.7

2. Design of TMD

Assuming the mass ratio

$$\mu = 0.03$$

Weight of TMD

$$W_d = W_s \times \mu = 134.4 \times 10^3 \text{ kN} \times 0.03 = 4032 \text{ kN}$$

Mass of TMD

$$m_d = \frac{W_d}{g} = 0.4112 \text{ kN.s}^2/\text{mm}$$

Optimum frequency ratio

$$\frac{\omega_d}{\omega_s} = \frac{1}{1+\mu} = \frac{1}{1.03} = 0.97$$

Circular frequency of TMD

$$\omega_d = 0.97 \times \omega_s = 0.97 \times \frac{2\pi}{T_s} = 0.97 \times \frac{2\pi}{1.28} = 4.766$$

Natural period of TMD

$$T_d = \frac{1.28}{0.97} = 1.318 \text{ sec}$$

Stiffness of TMD

$$K_d = m_d \omega_d^2 = 0.4112 \times 4.76^2 = 9.34 \text{ kN/mm}$$

Optimum damping factor

$$h_{opt} = \sqrt{\frac{3\mu}{8(1+\mu)^3}} = 0.101$$

Damping coefficient of TMD

$$C_d = \frac{2h_{opt}}{\omega_d} K_d = 0.398 \text{ kN.s/mm}$$

Story height of TMD

$$6 \text{ m}$$

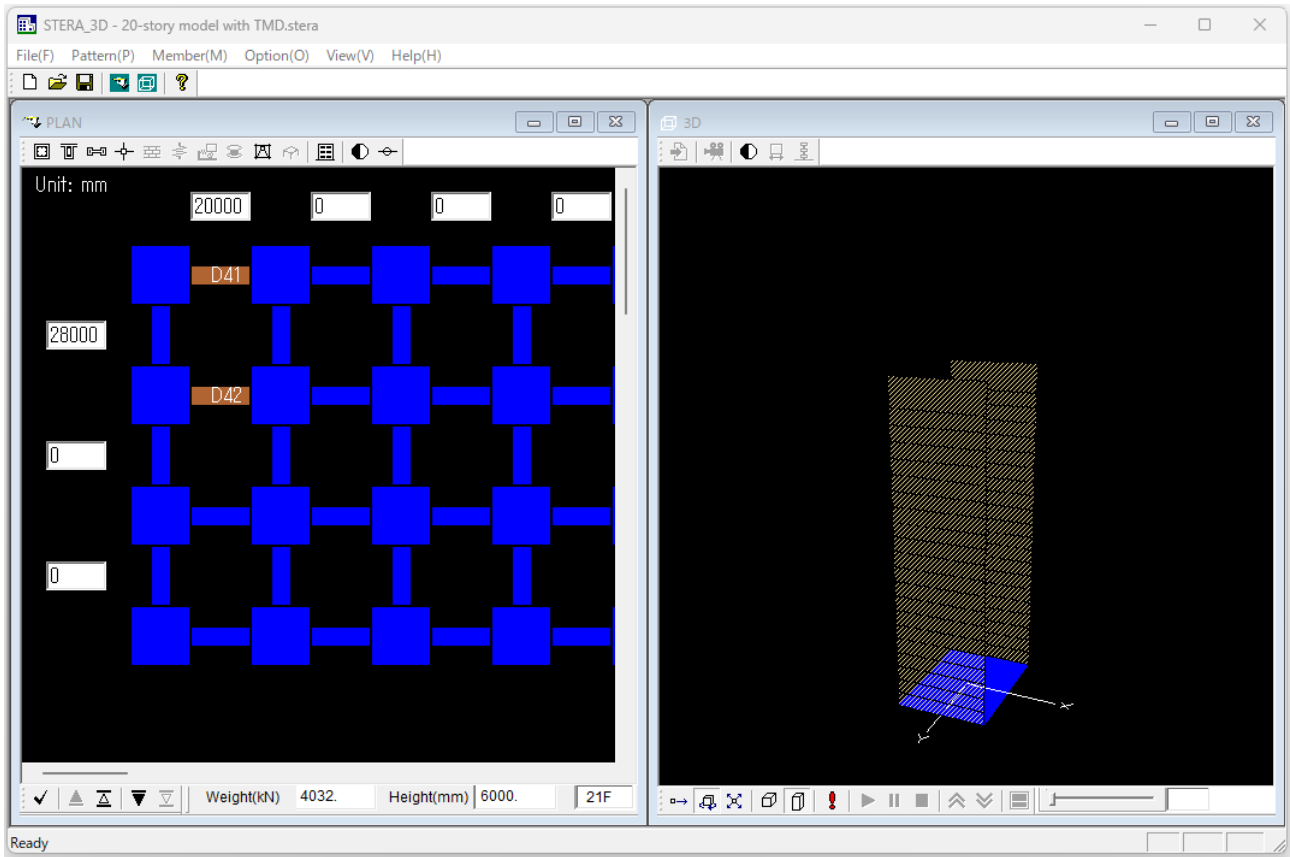


Figure 2 Analysis model of the building with TMD (20-story model with TMD.stera)

Table 2 Properties of TMD

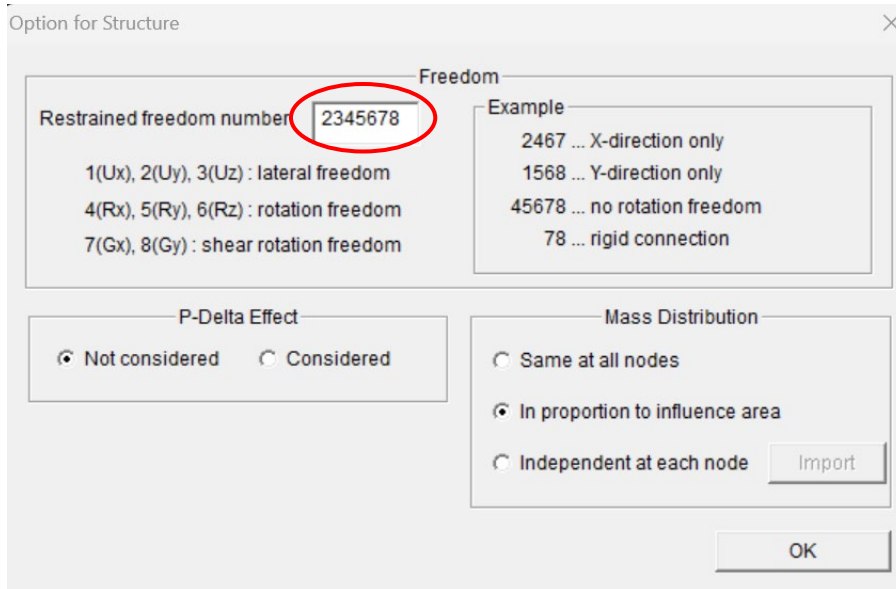
Story	Height (mm)	Weight (kN)	K (kN/mm)	C (kN.s/mm)
1	6000	4032	9.34	0.398

3. Input procedures of STERA_3D

Step 1. Restrained freedom number

Option > Structure

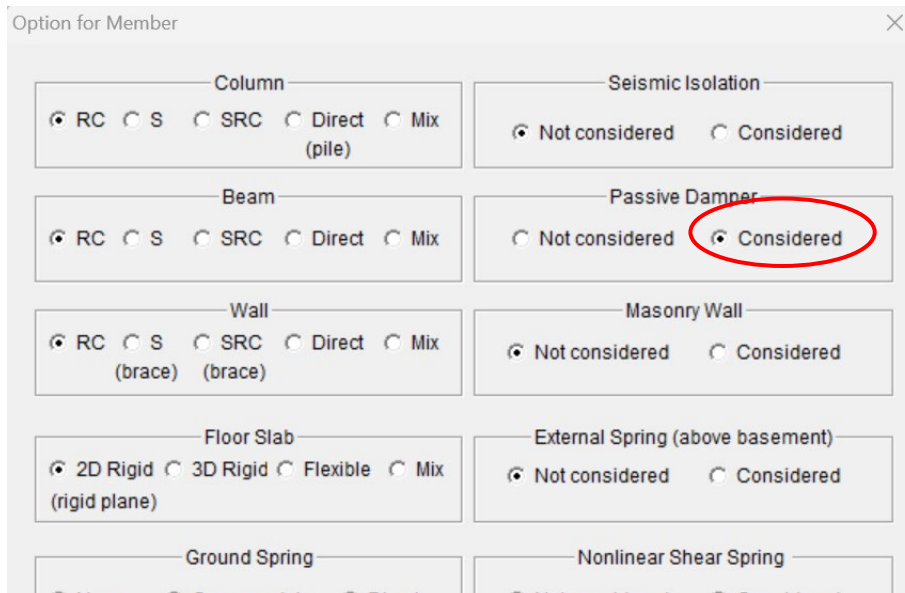
Since the direction of freedom is only X-direction (1), set “Restrained freedom number” to be 2345678.



Step 2. Passive damper

Option > Member

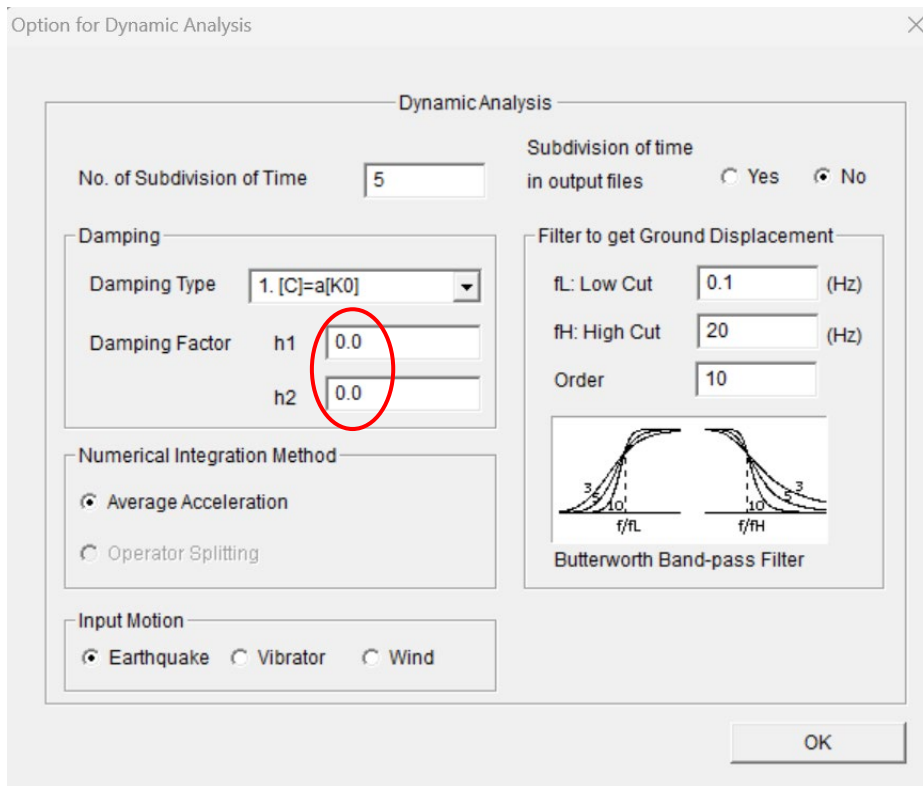
Since the passive damper is used for the lateral spring, set “Passive Damper” to be Considered.



Step 3. Damping factor

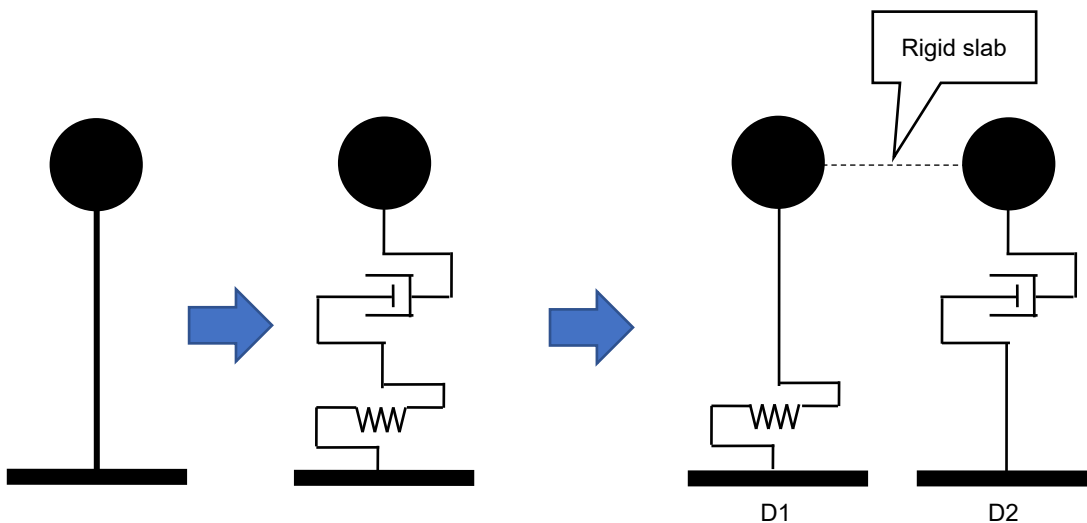
Option > Analysis > Dynamic

Since the damping property is given for each individual element, the viscous damping factors, h_1 and h_2 , are set to be zero.

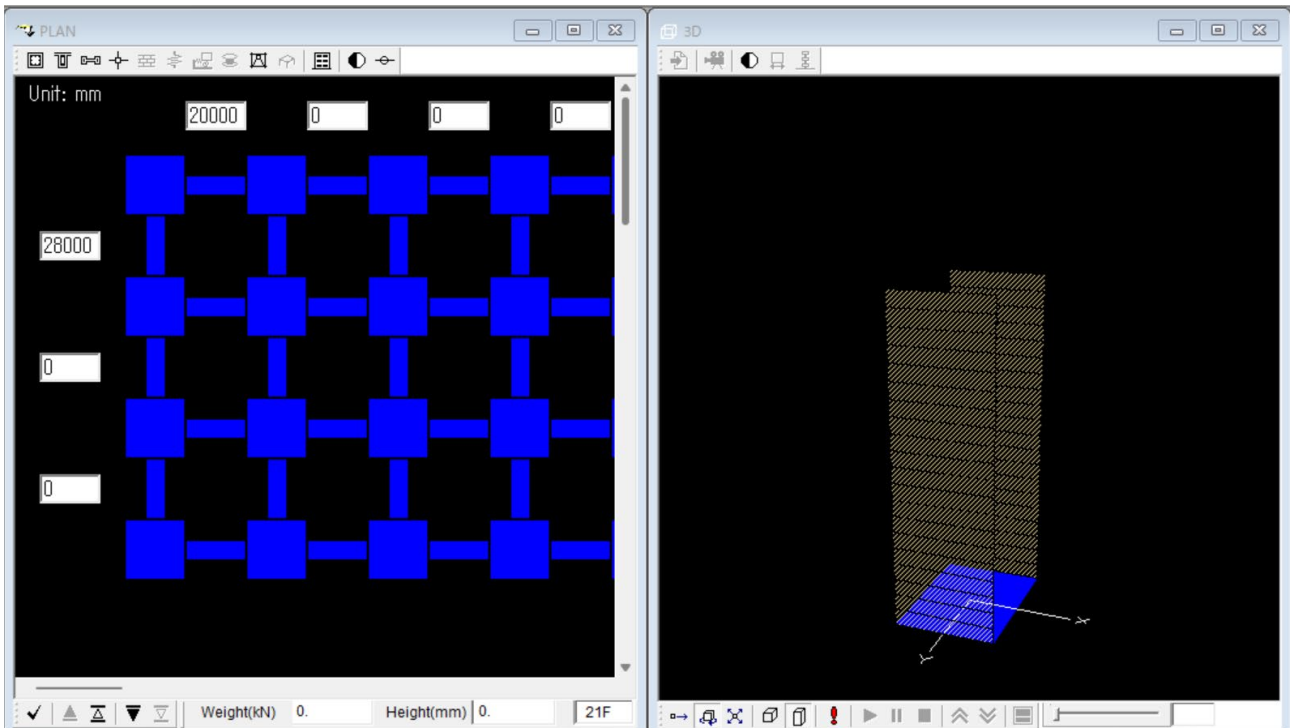


Step 4. Member setting (Main Building)

One story consists of two passive dampers (D1 and D2) with D1 as a spring member and D2 as a damping member.

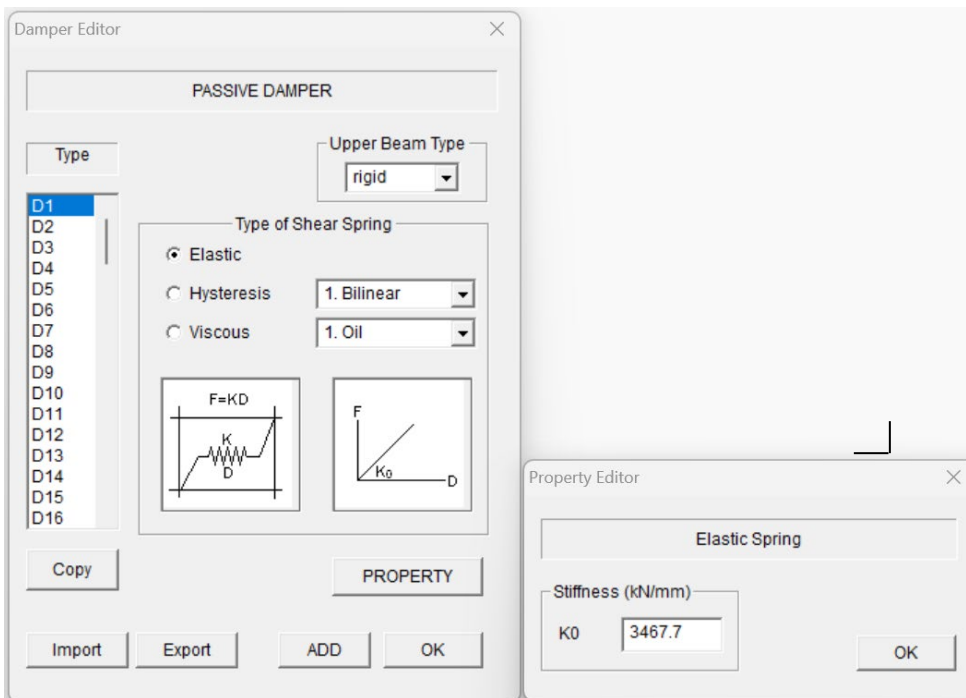



X-span 20000 mm, Y-span 28000mm, Story Weight 6720 kN, Story Height 3200 mm
 Continue to create up to 20th floor (D1~D40)



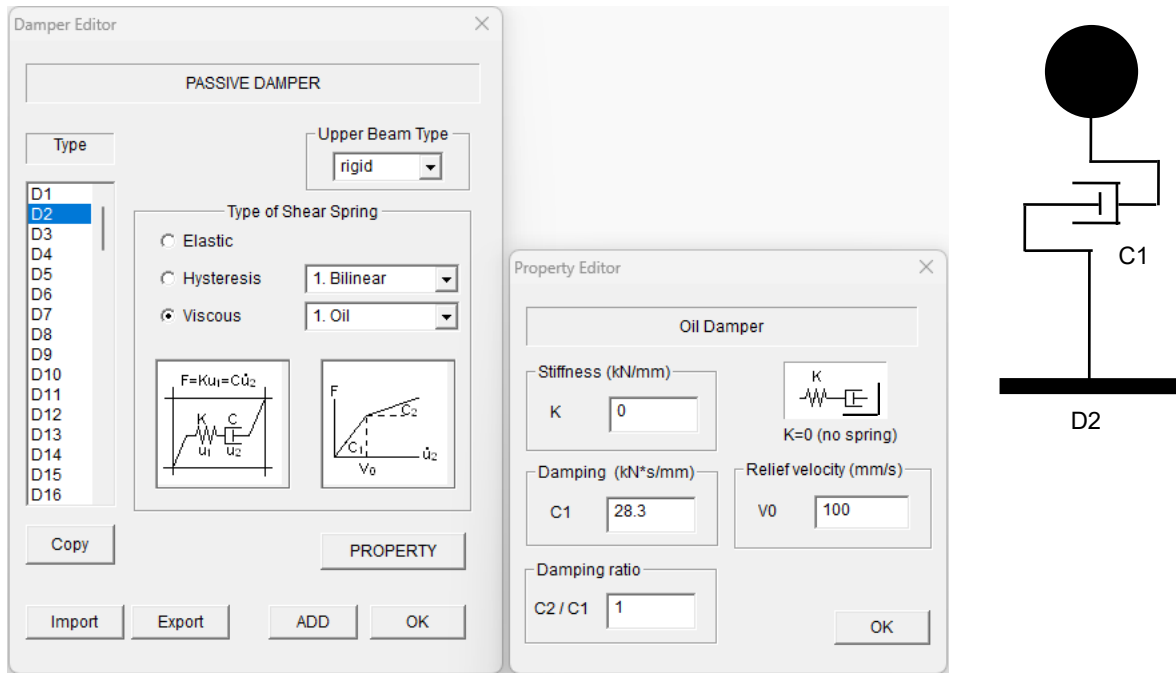
Passive dampers D1, D3, ..., D39 

Select type of shear spring to be “Elastic”, and input the stiffness K0 in “PROPERTY” window.



Passive dampers D2, D4, ..., D40 

Select type of shear spring to be “Viscous” and input the damping coefficient C1 in “PROPERTY” window. Other parameters, stiffness $K=0$, Damping ratio $(C2/C1)=1$, Relief velocity $V0=100$ mm/s.



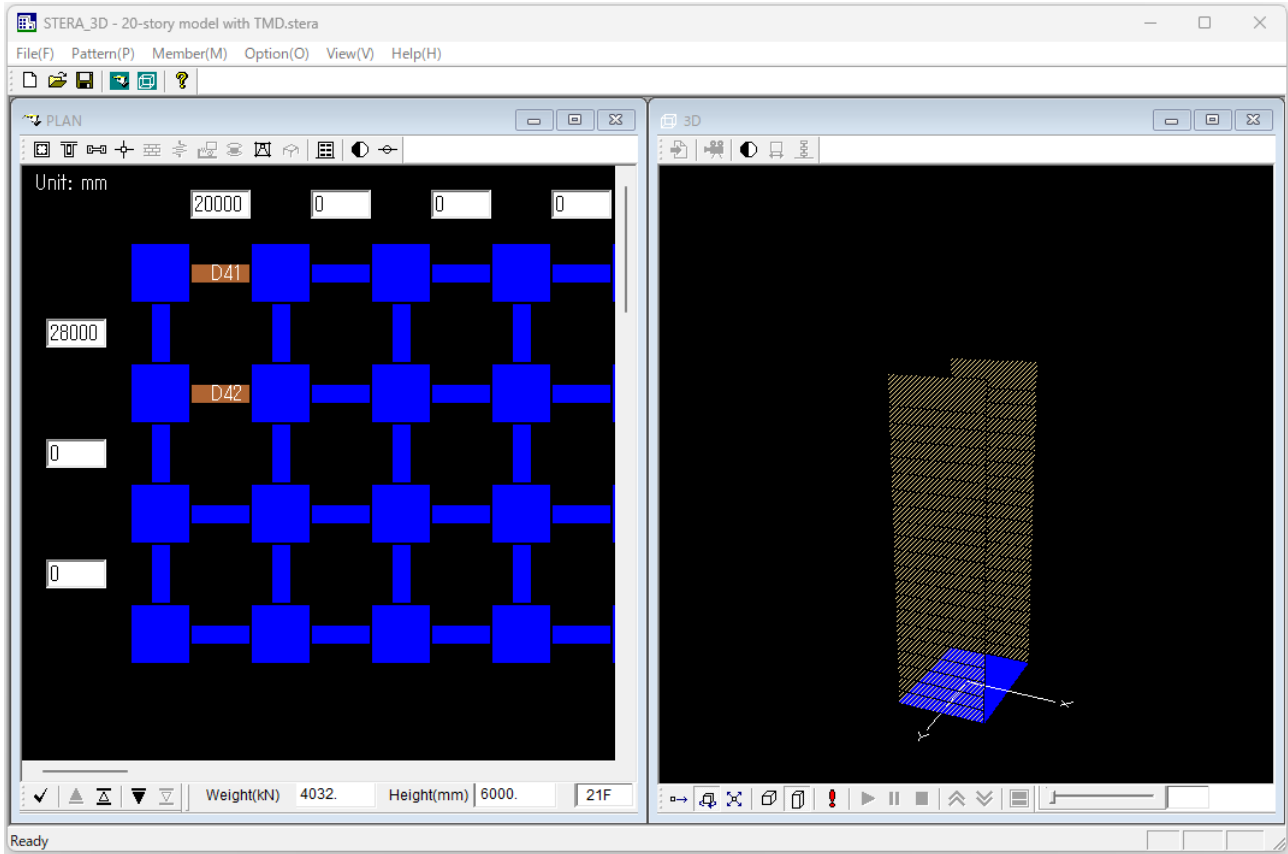
The image shows two software windows and a schematic diagram. The **Damper Editor** window is titled "PASSIVE DAMPER" and has a list of damper types (D1-D16) on the left, with D2 selected. The "Type of Shear Spring" section has three radio buttons: "Elastic", "Hysteresis", and "Viscous" (which is selected). The "Viscous" option has a dropdown menu set to "1. Oil". Below this are two graphs: the left one shows a linear relationship $F = K u_1 + C \dot{u}_2$ with a spring and damper symbol; the right one shows a bilinear hysteresis loop with parameters C_1 , C_2 , and V_0 . The "PROPERTY" button is visible at the bottom right of this window. The **Property Editor** window is titled "Oil Damper" and contains the following fields: "Stiffness (kN/mm)" with $K=0$; "Damping (kN*s/mm)" with $C1=28.3$; "Damping ratio" with $C2/C1=1$; and "Relief velocity (mm/s)" with $V0=100$. A schematic diagram to the right shows a mass (black circle) connected to a damper symbol labeled C1, which is in turn connected to a fixed base labeled D2.

Save the input data in the file “20-story model without TMD.stera”.

Step 5. Member setting (TMD)

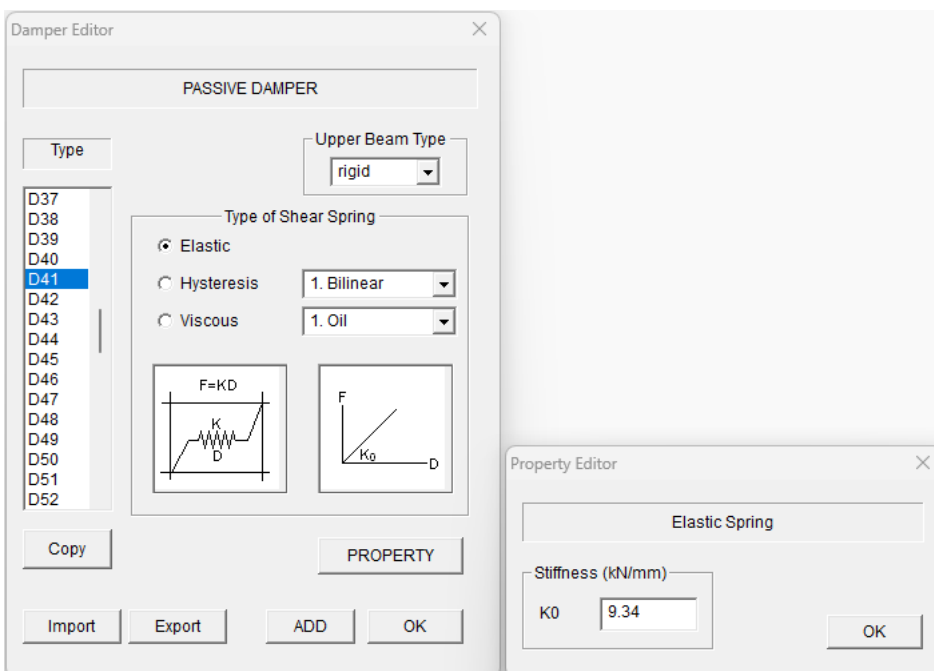
Create a TMD model for one floor above the main building (21st floor) with D41 as a spring member and D42 as a damping member.

Assume that the weight of the floor is 4032 kN and the height of the floor is 6000 mm.



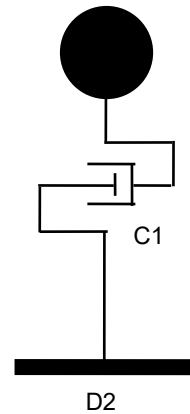
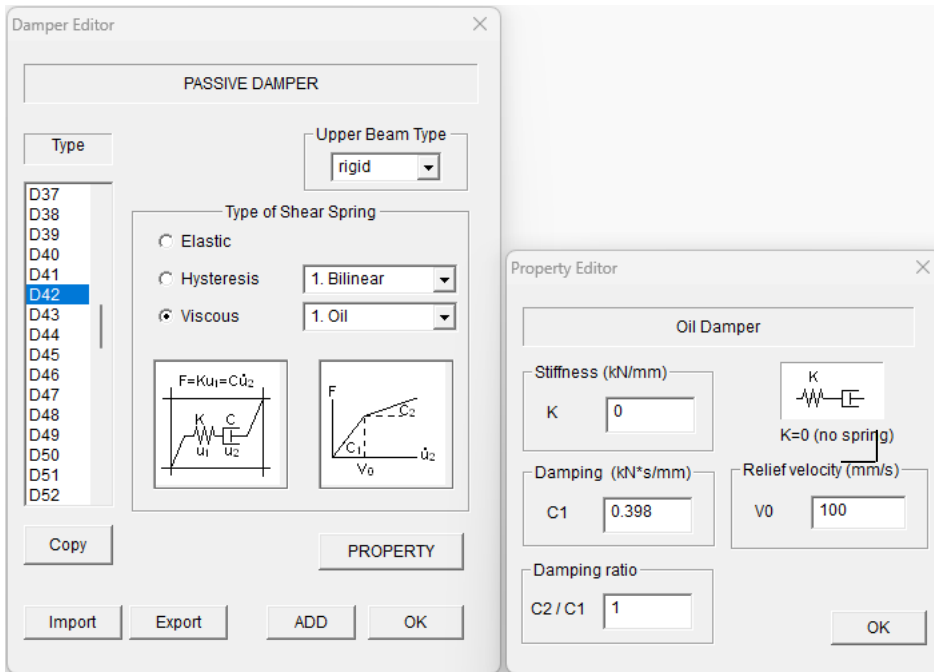
Passive damper D41

Select type of shear spring to be “Elastic”, and input the stiffness K_0 in “PROPERTY” window.



Passive damper D42

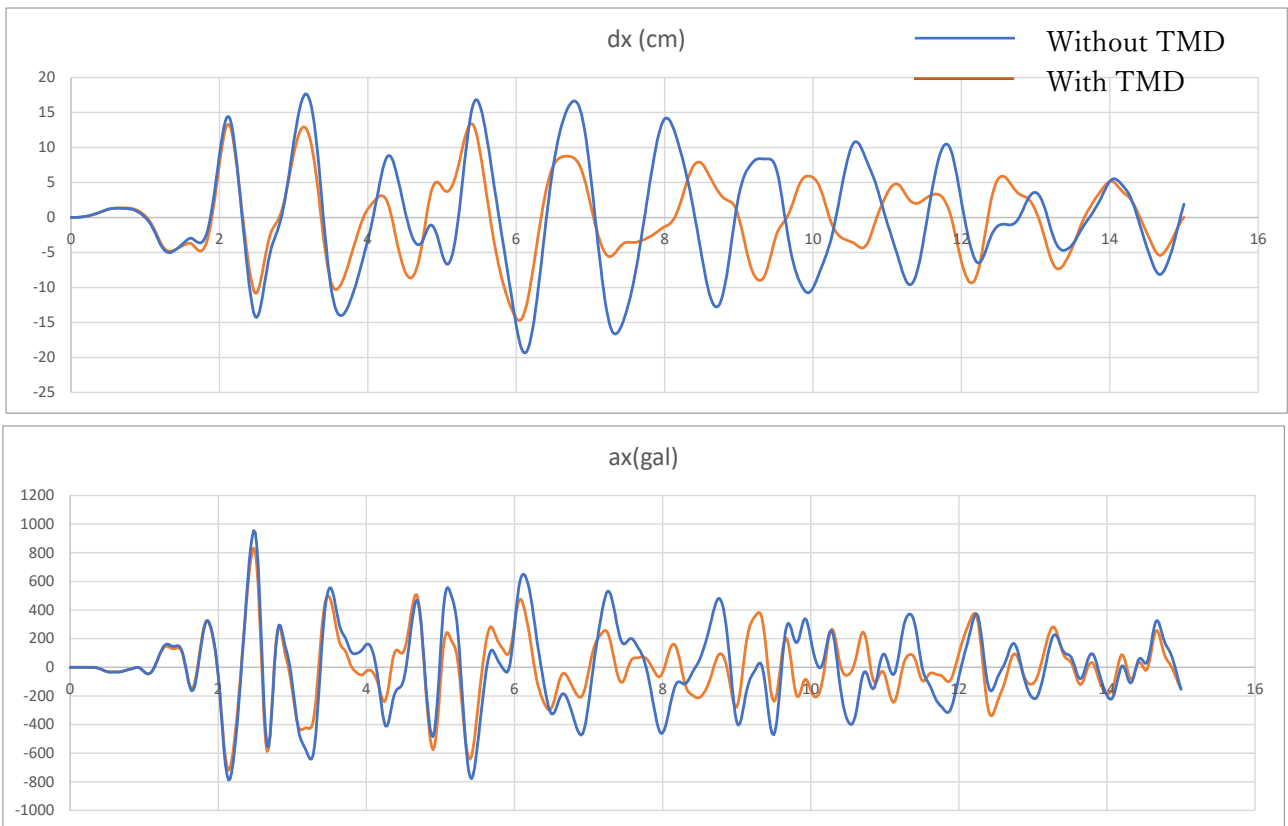
Select type of shear spring to be “Viscous” and input the damping coefficient C1 in “PROPERTY” window. Other parameters, stiffness $K = 0$, Damping ratio $(C2/C1) = 1$, Relief velocity $V0 = 100$ mm/s.



Save the input data in the file “20-story model with TMD.stera”.

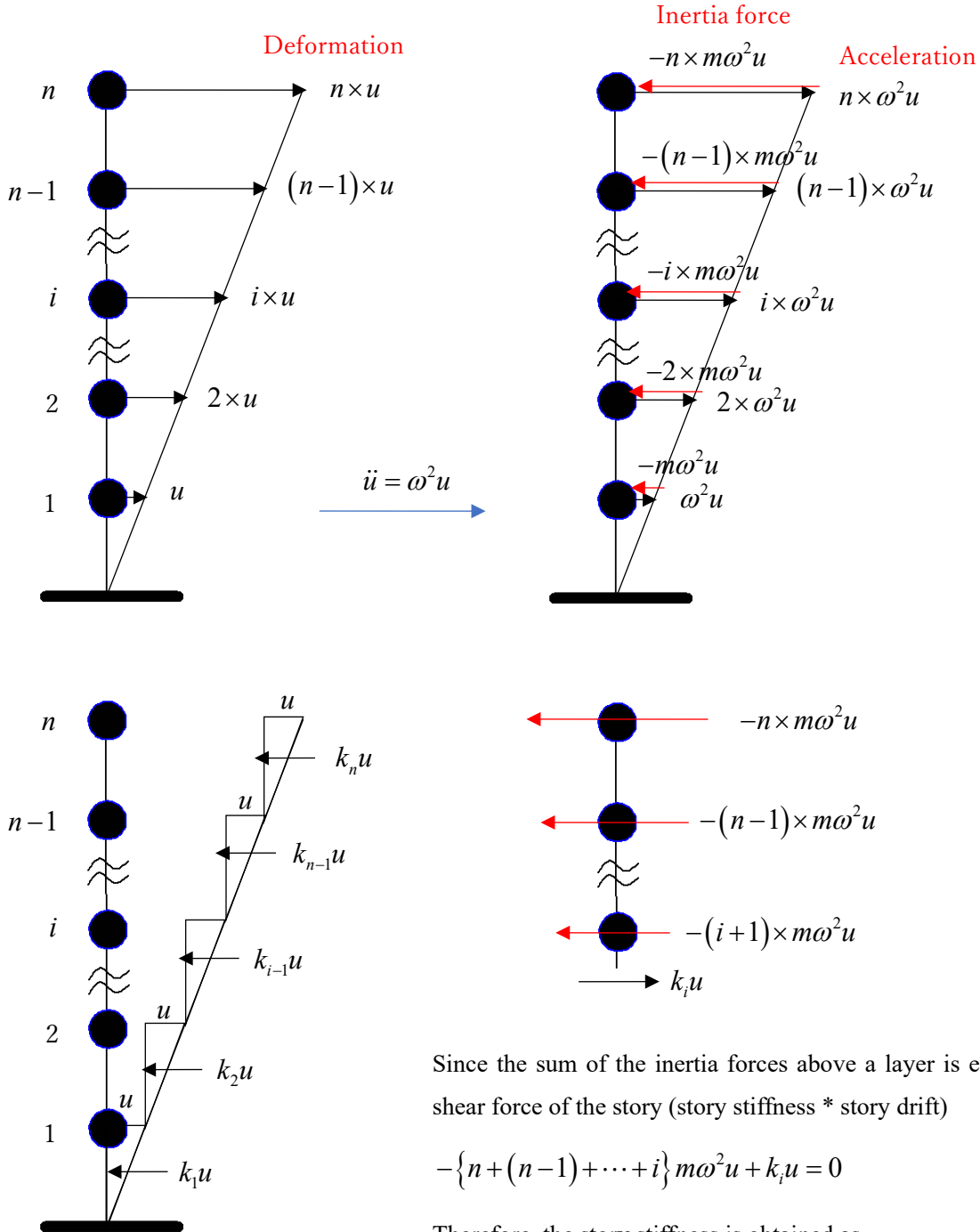
Step 6. Comparison of responses between the buildings with and without TMD

Displacement and acceleration responses at the 20th floor of the buildings with and without TMD under the El Centro 1940_NS earthquake wave are compared.



APPENDIX: Calculation of the story stiffness under an inverted triangle mode shape

Consider a building swaying with a first natural frequency ω and an inverted triangle natural vibration mode shape. The distributions of deformation, acceleration and inertia force (acceleration multiplied by the mass of each layer) are presented below.



Since the sum of the inertia forces above a layer is equal to the shear force of the story (story stiffness * story drift)

$$-\{n + (n-1) + \dots + i\} m\omega^2 u + k_i u = 0$$

Therefore, the story stiffness is obtained as

$$k_i = \{n + (n-1) + \dots + i\} m\omega^2 = \frac{1}{2} \{n(n+1) - i(i-1)\} m\omega^2$$